Building damage by the 2011 off the Pacific coast of Tohoku earthquake and coping activities by NILIM and BRI collaborated with the administration

Isao Nishiyama (NILIM), Hiroshi Fukuyama (BRI), Yasuo Okuda (BRI), and Izuru Okawa (BRI).

NILIM: National Institute for Land & Infrastructure Management BRI: Building Research Institute

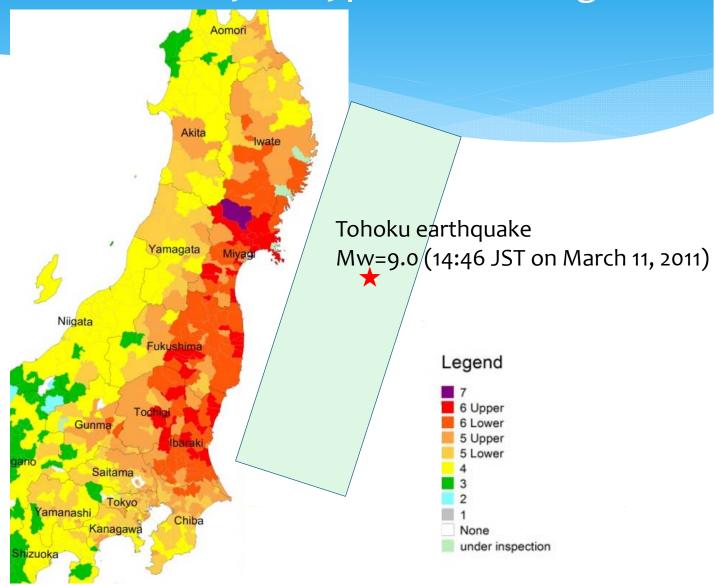
1. Outline

By Nishiyama, Isao

Field Survey

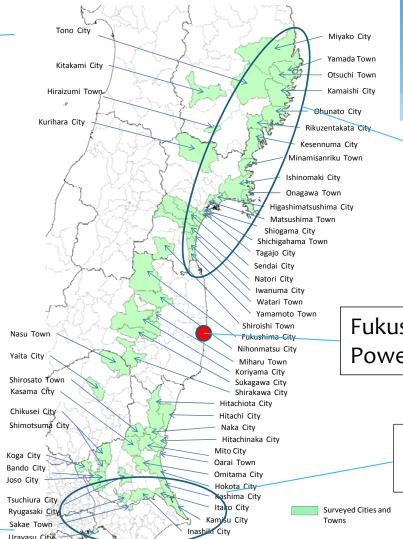
Quick Report (in Japanese) was published on May, 2011 and Summary Report (in English) will soon be available.

JMA Seismic Intensity & Hypocentral Region



Field Surveyed Cities and Towns

Motion-induced damage



Tsunami-induced damage

Fukushima Daiichi Nuclear Power Station

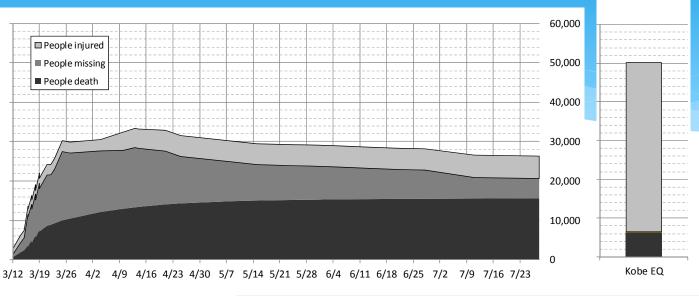
Liquefaction-induced damage of houses

Surveyed Items

- * Motion-induced damage
 - * Wood houses, steel buildings, reinforced concrete buildings, residential land, non-structural elements, seismically isolated buildings,... etc.
- * Tsunami-induced damage
 - * Wood houses, steel buildings, reinforced concrete buildings.
- * (Fire-induced damage...)

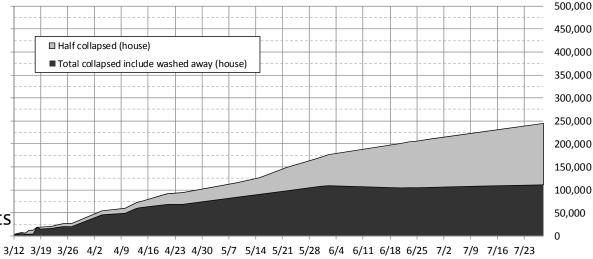


Damage Statistics (Tohoku vs. Kobe)



People Death Tohoku: 15,700 Kobe: 6,434

Total Collapsed Buildings
Tohoku: 114,000 houses
Kobe: 186,175 housing units



Kobe EQ

(housing

units)

Coping Activities

Four Important Issues

- Tsunami Damage
- * Non-structural Elements Damage, esp. Ceiling
- Long-period, Long-duration Ground Motion Effects
- Liquefaction Damage
- (Damper Damage in Seismically Isolated Building)

Tsunami



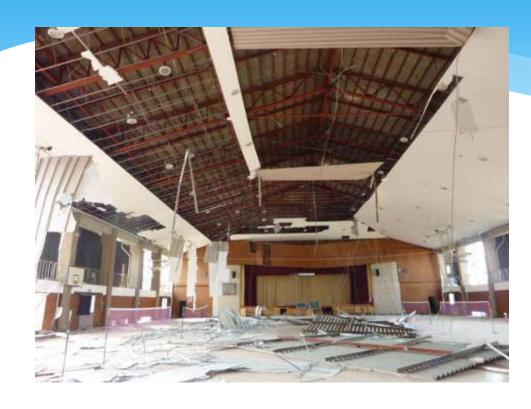


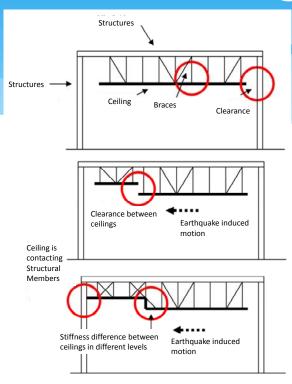


* Study on the design of tsunami evacuation buildings, i.e. estimation of tsunami load

More than half of the total inundation area was subjected to inundation height of 2m or less.

Non-structural Elements, esp. Ceiling

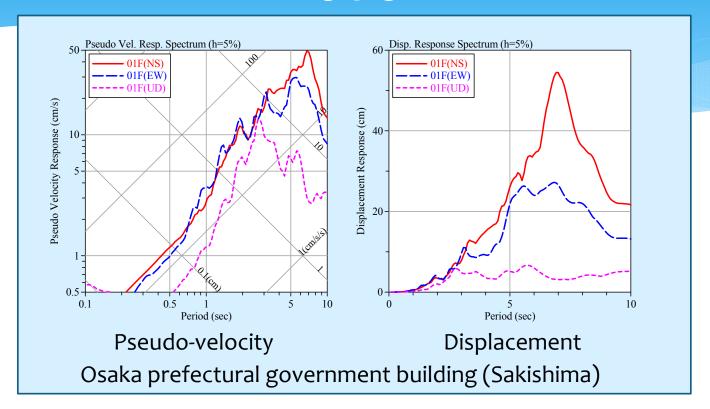




Previous technical advice (MLIT, 2003.10)

 Review of previous technical advice (right), and study on practical structural calculation methods

Long-period, Long-duration Ground Motion



- * Tentative new proposal by MLIT and NILIM was announced for public comments Dec. 21, 2010. 3 months before Tohoku EQ.
- * Background information was published in BRI.

Liquefaction





* Study on possible indication of expected performance w/wo countermeasures for residential houses (from the view of consumer protection)

(Damper in Seismically Isolated Bldg.)







LRB (Lead rubber bearing)?

Isao Nishiyama

Countermeasures in Codes/Standards

Building Structural Codes/Standards Committee

Chaired by Tetsuo Kubo, Tokyo University
Field Survey on the Earthquake on April 21 and 22
First meeting was on June 8, second on August 18

Draft of Building Structural Codes

WG on Long-period earthquake ground motion

First meeting was on July 20

Secretariat for supporting Committee and WG

TG on Building Structural Codes and Standards in general

First meeting on July 26

Public comments on Tentative New Proposal of countermeasures for long-period motion

Collection of information by using grant-in-aid for maintenance and promotion of building standards

42.Effect of long-period motion on super high-rise buildings

21. Needs and seeds collection

Public comments or proposal of building structural codes from private

Isao Nishiyama

2. Building Damage due to Earthquake Ground Motions

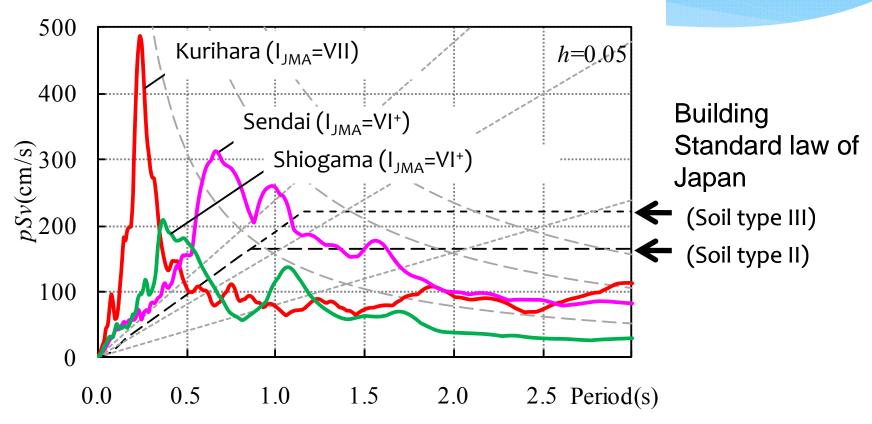
By Fukuyama, Hiroshi

Damage to buildings caused by seismic motion ¹⁷ <Summary>

Damage to buildings is not so severe whereas the seismic intensities were high and the disaster areas were extended to extremely large

- Wood Structure: Typical seismic damage was observed
- RC Structure, Steel Structure: Significant difference appears between before and after the new seismic design code (1981). Typical seismic damage was observed
- Non-structural Elements: Fall of suspended ceilings in large-scale spaces, exterior walls, and interior materials were observed
- Residential Land: Damage to developed grounds and sloping for residential houses were observed. Severe liquefaction damage occurred in very wide areas.

In Kurihara City, JMA seismic intensity of VII was recorded, predominant spectrum is observed in short period, i.e. less than 0.3s. But the power of spectrum in long period is lower than the limit value regulated in Building Standard Law of Japan for seismic design. Building damage was not so significant on the whole even in the areas where seismic intensity of more than VI was recorded



Pseudo-velocity response spectrum at some K-NET observe points Hiroshi Fukuyama



Damage of houses with store (Inclination of 1st story)



Damage due to Bio-deterioration



Damage of Dozo (Japanese traditional wood storehouse coated with clay and plaster finish)



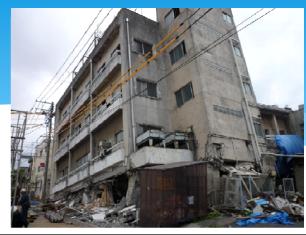
Collapse of 1st story



Collapse of 2nd story

Hiroshi Fukuyama

Typical seismic damage to RC Structures 20



Collapse of soft-1st story by shear failure of columns



Shear failure of non-structural walls



Pullout of anchor bolts of the exposed-type SRC column base



Shear failure of link-beam



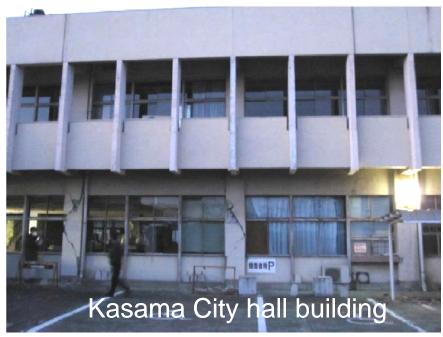
Shear failure due to opening of shear wall

Typical seismic damage – RC structure (1)

• More than 10 local government office buildings designed by the old seismic code suffered from significant structural damage, shear failure of short columns and loss of axial load bearing capacity.

These building could not be used as an emergency operation center.

• Damage mitigation for functional continuity is strongly required.





Hiroshi Fukuyama

Typical seismic damage – RC structure (2)

- Most of the retrofitted buildings performed well to secure human lives by preventing collapse.
- Damage were observed in some retrofitted buildings





Typical seismic damage – RC structure (3)



Courtesy of Mr. K. Watanabe of U.R.

Hiroshi Fukuyama

Typical seismic damage to Steel Structures 24



Buckling of brace



Rupture of horizontal brace



Spalling of concrete at joint



Rupture of brace at joint

Buckling of diagonal member of latticed column







Hiroshi Fukuyama

Typical seismic damage to Residential Land²⁵







Large-scale liquefaction and settled or tilted structures

Sand boiling and tilting of house



Failure of hooting caused by the ground damage



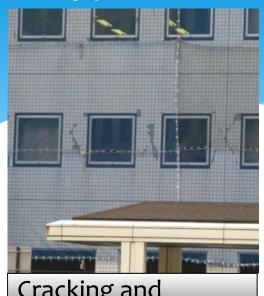
Land sliding on the slope of the developing hill



Damage of retaining wall and house movement

Hiroshi Fukuyama

Typical damage to Non-structural Elements²⁶



Cracking and spalling of tile



Failure of glass



Fall of exterior wall panels







Damage and fall of suspended ceiling

Typical damage to Seismically Isolated Buildings²⁷



Damage to cover-panels for fire protection

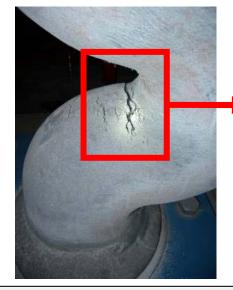


Damage to expansion joint



Peeled off of paint on U-shape dampers







Lead damper and crack on the surface

Countermeasures

Most of the damage classified were observed in the previous earthquakes. Then previous revising of codes (or handbook) are effective for preventing the damage.

However, fall of suspended ceilings in large-scale spaces, liquefaction damage, and damper damage in seismically isolated building are forced to take prompt measures.

Detailed investigation on damage to retrofitted buildings and government office buildings are now on-going.

3. Damage to Buildings in Inundation Areas due to Tsunami

By Okuda, Yasuo

Purpose of Investigation

The purpose of this investigation is

- 1) To understand an overview of buildings damaged by tsunami,
- To obtain basic data and information required to evaluate mechanisms for causing damage to the buildings
- To contribute to tsunami load and tsunami-resistant designs for buildings such as tsunami evacuation buildings

by means of

- 1) collecting building damage cases by tsunami
- classifying the damage patterns for different structural categories,
- 3) making a comparison between the calculated tsunami force acting on buildings and the strength of the buildings

Investigation Team for Tsunami Damage

NILIM: 8 members

Isao Nishiyama

Akiyoshi Mukai

Ichiro Minato

Atsuo Fukai

Shuichi Takeya

Hitomitsu Kikitsu

Hiroshi Arai

Tomohiko Sakata

BRI: 19 members

Juntaro Tsuru Nobuo Furukawa

Masanori liba Shoichi Ando

Wataru Gojo Hiroshi Fukuyama

Yasuo Okuda Taiki Saito

Bun-ichiro Shibazaki Koichi Morita

Hiroto Kato Tsutomu Hirade

Takashi Hasegawa Tadashi Ishihara

Norimitsu Ishii Yushiro Fujii

Haruhiko Suwada Yasuhiro Araki

Toshikazu Kabeyasawa

Summary of Damage in Inundation Area Due to Tsunami

- about 106,000 houses were completely destructed or missing mainly in Iwate, Miyagi and Fukushima prefectures
- about 100,000 houses were partially damaged
- 3. about 106,000 houses were below partially damaged

Total: about 370,000

		Human Damage			House Damage			
Prefecture	City, Town, Village	Dead	Missing	Injury	Complete Destruction or Missing	Partial Damage	Below Partie Damas	Fire
Aomori	Hachinohe	1.	1		250	769		
	Hashikami	0	0	0	12	8	1	
	Total	1	1	17	262	777	1	2
Iwate	Hirono	0	0	0	10	16	5	
	Kuji	2	2	8	65	210		
	Noda	38		17	309	169		
	Hudai	0	1	1				
	Tanohata	14	19	8	225	45	4	
	Miyako	420	124	33	3,669	1,006	176	
	Yamada	597	256	Unknown	2,789	395	120	
	Otsuchi	796	653	Unknown	0.400	3,677		
	Kamaishi	881	299	Unknown	3,188	535	120	
	Ofunato	331	118	Unknown	3,6		Unknown	
	Rikuzentakata	1,546	569	Unknown	3,159	182	27	
	Total	4,625	2,041	67	20,720	2,558	452	1
Miyagi	Kesen-numa	1,004	410	Unknown	8,533	2,313	3,248	
	Minamisanriku	550	437	Unknown	3,167	144	Unknown	
	Onagawa	535	414	2	2,939	337	640	
	Isinomaki	3,153	890	Unknown	19,065	3,354	10,199	2
	Higashimatsushima	1,044	104	Unknown	4,589	4,672	2,471	
	Matsushima	2	0	37	213	1,321	1,184	
	Rifu	1	1	1	59	508	1,732	
	Shiogama	20	1	10	682	2,784	3,973	
	Shichigahama	66	6	Unknown	729	460	1,067	
	Tagajo	188	3	Unknown	1,662	2,993	5,097	1
	Sendai	704	33	2,276	19,922	41,344	56,347	3
	Natori	911	82	Unknown	2,786	922	8,060	1.
	Iwanuma	183	1	293	720	1,545	2,403	
	Watari	256	5	44	2,459	1,032	1,985	
	Yamamoto	670	23	90	2,200	1,042	1,086	
	Total	9,287	2,410	2,753	69,725	64,771	99,492	12
Fukushima	Shinchi	107	3	3	548	Unknown		
	Soma	454	5	71	1,049	643	3,092	
	Minamisoma	633	38	59	4,682	975		
	Namie	141	43					
	Futaba	29	6	1	58	5		
	Okuma	73	1		30			
	Tomioka	19	6					
	Naraha	11	2	5	50			
	Hirono	2	1		Unknouwn	Unknown		
	Iwaki	308	39	4	6,585	18,931	21,800	
	Total	1,777	144	143	13,002	20,554	24,892	
Ibaraki	Kitaibaraki	5	1	188	339	1,569	5,745	
	Takahagi	1		19	131	728	3,213	
	Hitachi			166	403	3,016	11,229	
	Tokai	4		5	56	104	3,150	
	Hitachinaka	2		27	79	720	5,863	
	Oarai	1		6	10	268	1,087	
	Hokota			15	96	524	4,863	
	Kajima	1			368	1,726	2,567	
	Kamisu			6	139	1,660	3,011	
	Total	14	1	432	1,621	10,315	40,728	2
Chiba	Choshi			19	23	105	1,938	
	Asahi	13	2	12	336	931	2,358	
Total		13 15,717	2	31	359	1,036	4,296	
	Sum Total		4,599	3,443	105,689	100,011	169,861	16:

Classification of Damage Patterns Reinforced Concrete Buildings (1) Collapse of first floor



A case where column capitals and bases on the first floor in a building were subject to flexural failure and subsequently to story collapse was seen in two-story buildings.

(2) Overturning



Overturning was observed in 4-story or lower buildings. In all overturned buildings, the maximum inundation depth exceeded their height. Overturning types include building that felt sidelong and buildings that turned upside down.

(3) Movement and washed away



Most of the overturned buildings were moved from their original positions. It is estimated that large buoyancy acted on the buildings. Moved and overturned buildings left no dragged traces on the ground.

(4) Tilting by scouring



When tsunami acted on a building, a strong stream was generated around the corner of the building, resulting in many large holes on the ground that were bored by scouring. In one case, a building on mat foundation fell into a hole bored by scouring.

(5) Fracture of wall



In one damaged building, a 300 mm-thick shear wall with double layer bar arrangement and a support span of more than 10 m and without no 2-story floor was bent inside by a tsunami wave pressure.

(6) Debris impact



Debris impact was seen in most of the non-structural members such as window and ceiling materials. The number of cases of clear damage to skeletons was not large, but in one observed case, a multi-story wall in an apartment house was probably bored by debris impact.

Classification of Damage Patterns Steel buildings (1,2) Movement and washed away





Debris impact was seen in most of the non-structural members such as window and ceiling materials. The number of cases of clear damage to skeletons was not large, but in one observed case, a multi-story wall in an apartment house was probably bored by debris impact.

(3) Overturning



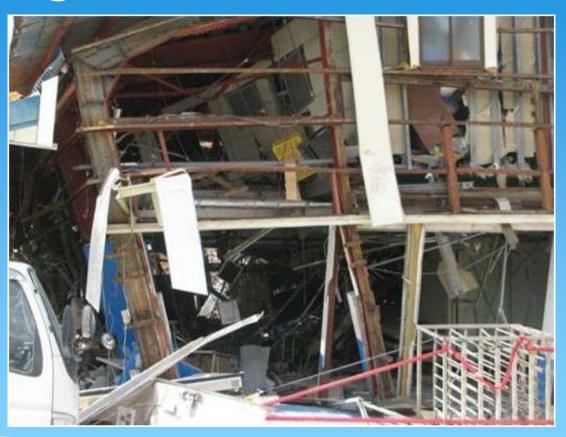
One case, in which a whole building including foundation is overturned, was confirmed. Most of the ALC panels of claddings were left.

(4) Collapse



Damage cases of skeleton collapse include story collapse of the first floor in a 2-story steel building and partial collapse of a warehouse on the coast.

(5) Large residual deformation



Slight tilting was often observed in steel buildings with only a skeleton left. In one case, a gabled roof frame building did not collapsed despite large residual deformation.

Yasuo Okuda

(6) Full fracture and washed away of cladding and internal finishing materials



Cladding materials such as ALC panel were almost fully fractured and washed away, and a steel frame as a skeleton was left. This case was often seen.

Damage to wood houses (1)



In the case of a maximum inundation depth more than about 6 m (equivalent to a height of eaves of 2-story wooden house), the number of 1-story and 2-story Wood Houses that remained was almost zero.

In the case of a maximum inundation depth of about 1 m, most of wood houses remained.

Damage to wood houses (2)





A tsunami wave force was reduced possibly due to many openings in the direction affected by tsunami or on the whole plane, or a wooden house remained despite washout of columns and external walls in the corner of the building.

Database for Investigated Buildings

Outer dimensions of about 100 buildings and dimensions of their skeletons were measured in the site investigation.

Building name, address, purpose, construction year, designation as tsunami evacuation building, structure category, number of stories, outer dimension, distance from seacoast (river), GPS position, altitude, surrounding circumstances, damage situations, etc., were included in the database.

建物番号	RT-12	[-12 調査日 2011年4月6日				
名称	診療所			Ver	500	
所在地	陸前高田市高田町馬場前			建設年 不明		
用途	病院・診療所			津波避難ビル 指定なし		
構造種別	S造 (ラーメン構造)					
建物規模	階数	3 階	(地下	階)	高さ:	9.6 ▅
	平面寸法	21.5 m ×		7 m		
建物位置	海岸からの距離	約1200 🛥	標高		5 m	(GPS)
	立地条件	陸前高田駅前交差点近く。平坦な市街地				
最大 浸水深		9 m		周辺建物の痕跡より		
津波後の状況	建物の状態	原位置に残存	1×5カ 体に指	1×5スパン、外装材が脱落しているが躯体に損傷は見られない		
		被害なし			vii	
	非構造部材の被害	被害あり	外装标	外装材の脱落		
備考			100			

- | 階柱口-300×300、桁行梁 H-300×150×6.5×9、梁間梁 H-396×199×7×11
- 津波作用面の反対側に隣接する RC 造 2階建て躯体の被害は軽微であった

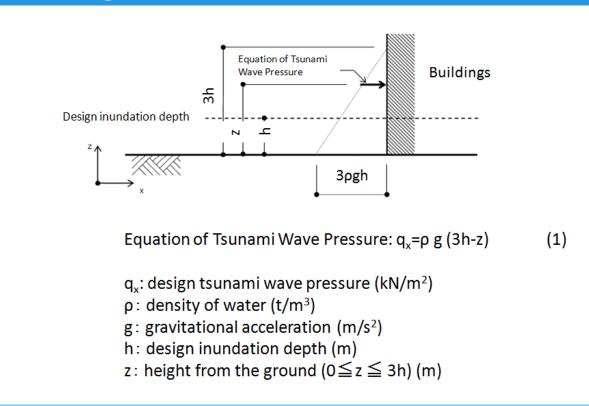






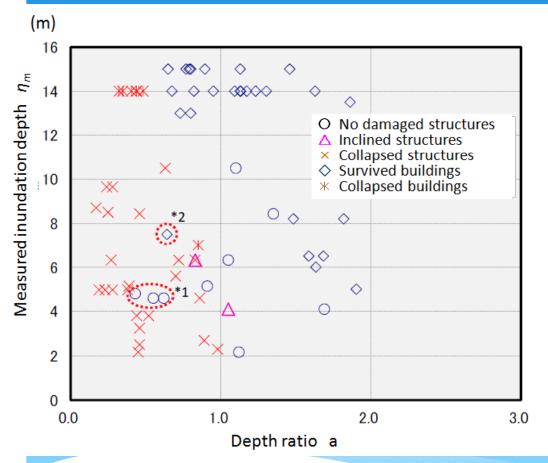


Discussion on Guidelines for Tsunami Evacuation47 Buildings by the Cabinet Office, Japan



In the Cabinet Office guidelines, the design tsunami load for the tsunami evacuation buildings was adopted as the tsunami wave pressure eq. (1), hydrostatic pressure of 3 times design inundation depth, based on the maximum envelope of the experimental result in Japan.

Damage Situations of Buildings and Structures 48 with Some Obstacles for Tsunami Effect



A depth ratio is defined as eq. (2).

$$a = \frac{\eta_e}{\eta_m} \tag{2}$$

a: depth ratio

 η_e : depth of the hydrostatic pressure equivalent to the strength of the buildings and structures (m)

 η_m : measured inundation depth (m)

This figure plots damage situations of buildings and structures with some obstacles for tsunami effect for a and η_m . A boundary line of damage situations of buildings and structures can be drawn at the depth ratio a =1 where η_m <10m.

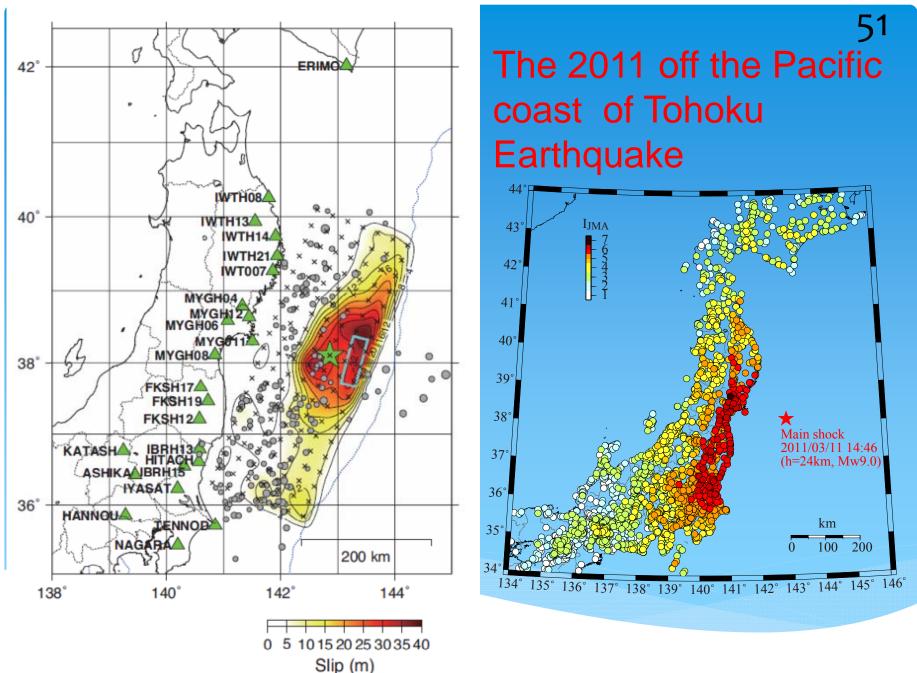
Conclusions

This section's conclusions are as follows;

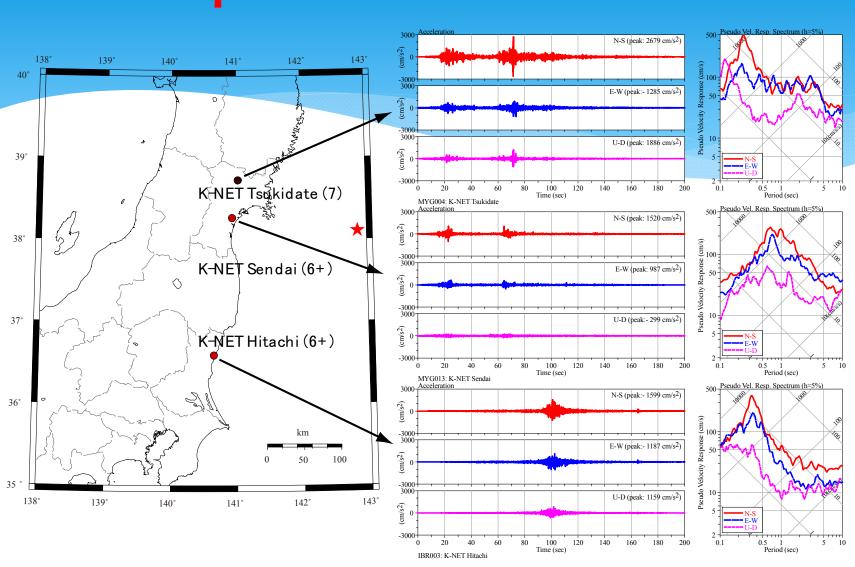
- The damage patterns for different structural categories were classified and the factors that had caused various types of damage were briefly discussed.
- 2) The database of the investigated buildings and structures was made.
- Based on the database, we plotted the damage situations of the investigated buildings and structures for the measured inundation depth and the depth ratio. A boundary line of damage situations of buildings and structures can be drawn at the depth ratio a = 1 where η_m <10m.

4. Ground Motions of the Tohoku earthquake and Recent Activity on Long-period Motions for Design of Building Structures

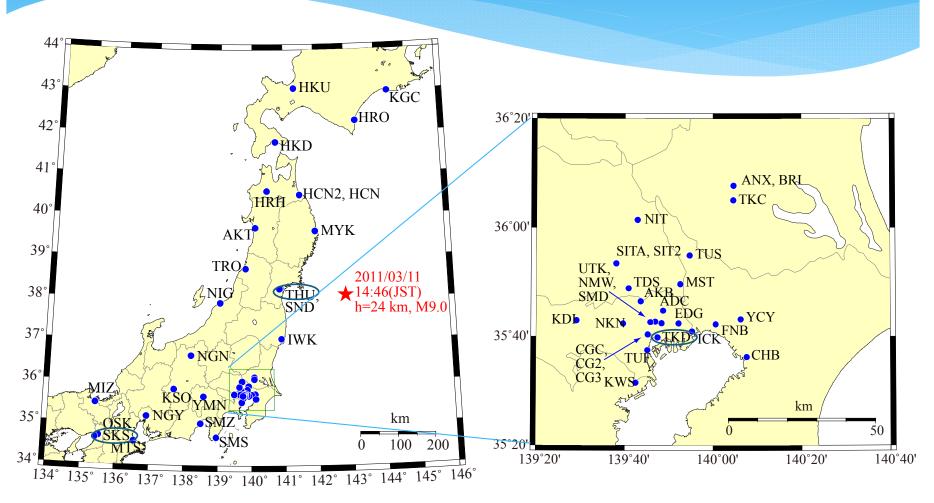
By Okawa, Izuru

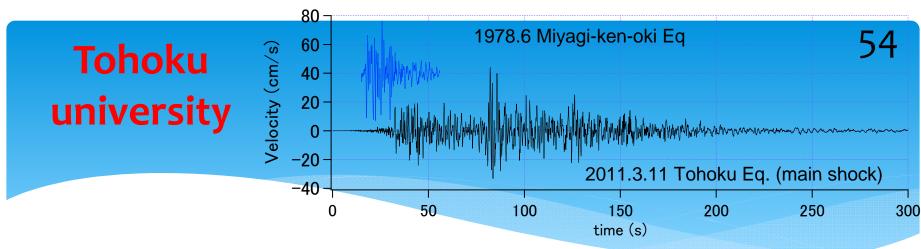


Examples of observed motions

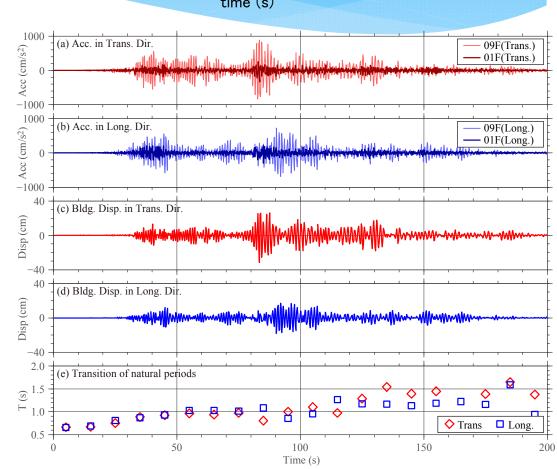


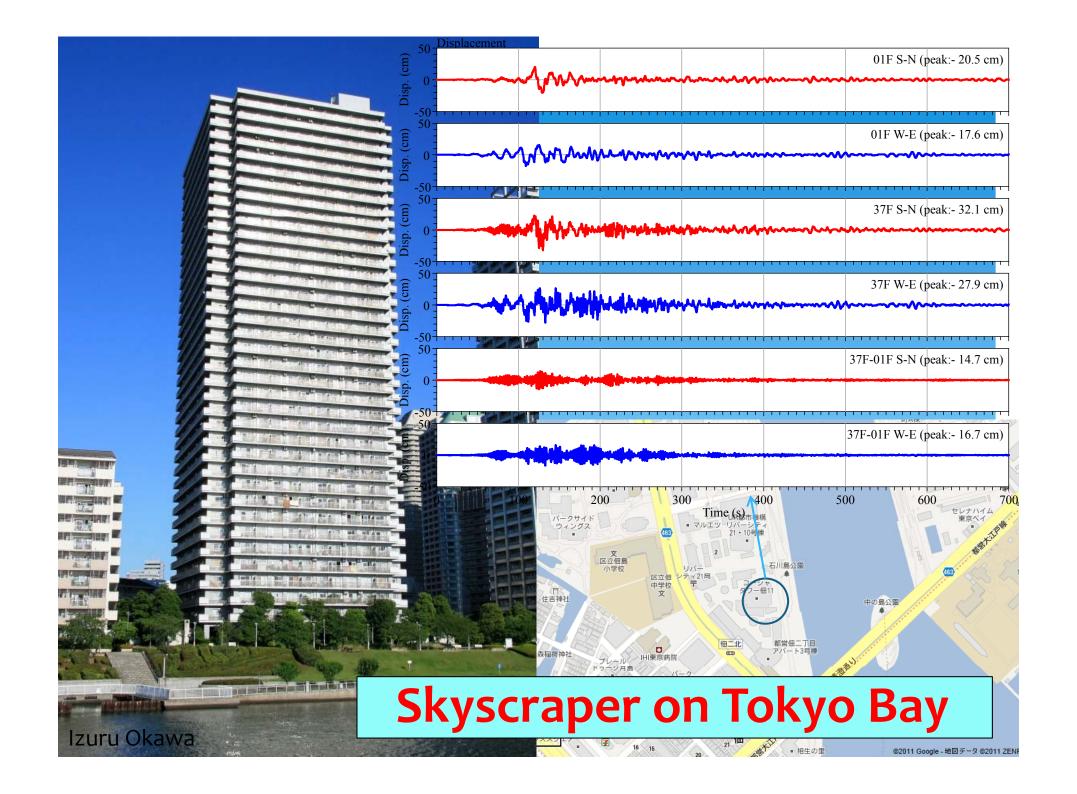
BRI Strong motion observation network (Instrumentation in Buildings)









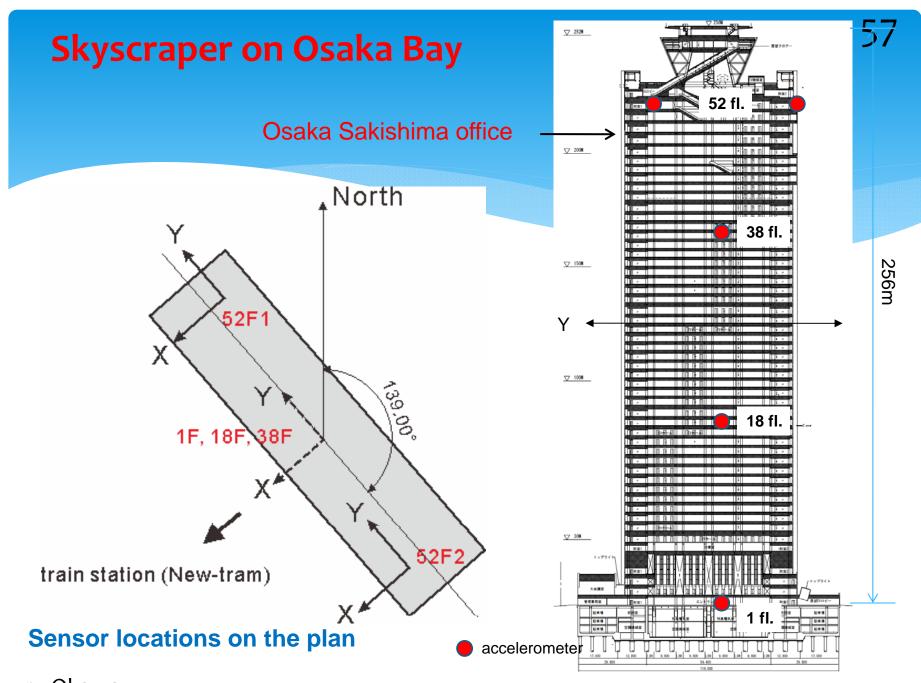


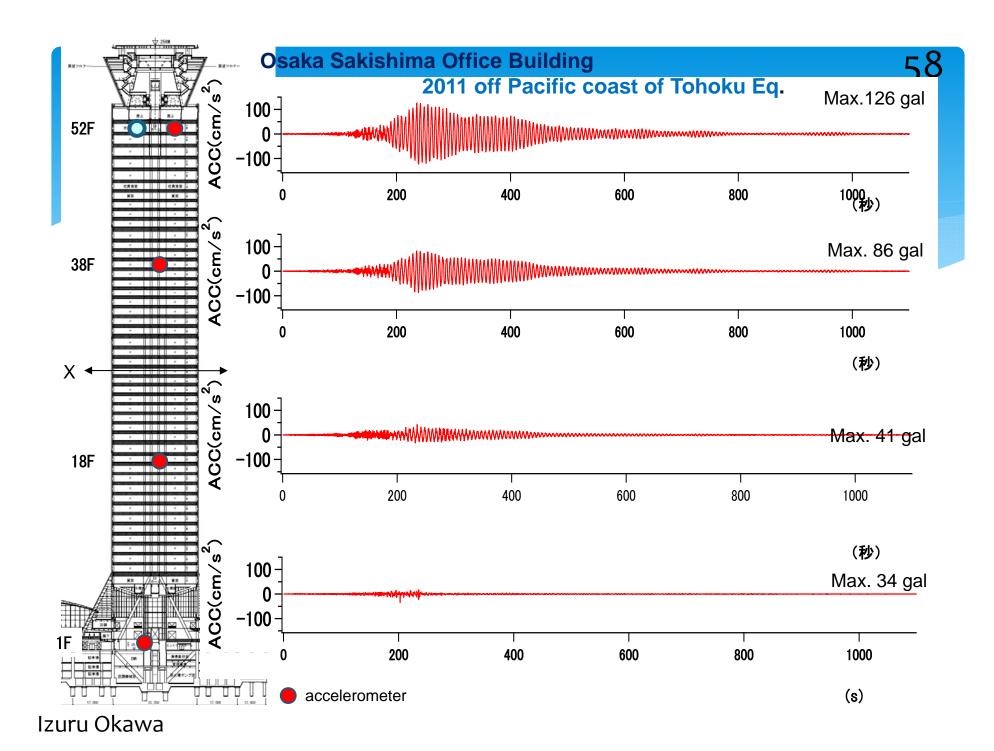
Skyscraper on Osaka Bay, tallest in western Japan, with more than 700 km epic. distance.

Osaka Sakishima office









140 h=0.05 Pseudo velocity spectrum Akita pref. office B1F 120 Hachinohe city hall GL eudo Velocity (cm/s) Iwaki city hall B1F of observed motions Miyako city hall GL 100 Niigata city hall B1F Sendai Gov. Bldg B2F - BSL design bedrock motion 43° HKU 42° 10 41 Period (s) HCN2, HC 40° 120 Adachi Gov. Bldg, 01F 39° University Bldg, Kasukabe_GL 100 - Saitama Gov. Bldg No.2, 01F 2011/03/11 Misata city hall, GL THU, SND 38° **★**14:46(JST) Pseudo velocity (cm/s) TUS, Noda, 01F h=24 km, M9.0 BSL design bedrock motion 37° NGN 60 36° 35 km 100 20 134° 135° 136° 137° 138° 139° 140° 141° 142° 143° 144° 145° 146°

Izuru Okawa

2

Period (s)

10

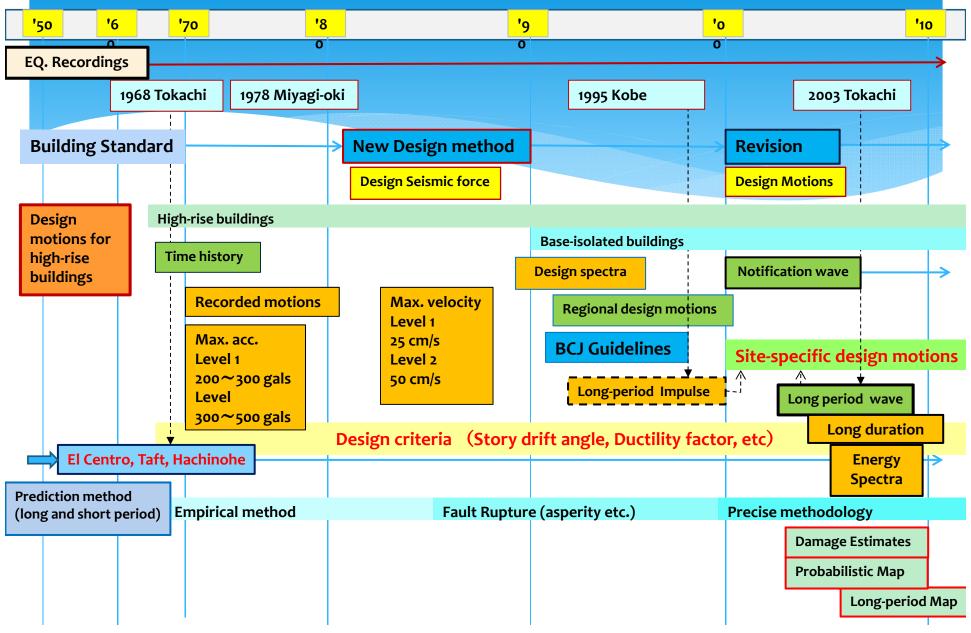
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MLIT & NILIM proposal for tentative measures for 60 the safety of high-rise buildings

Background

- * Fire of large oil storage tank due to the effect of long-period earthquake motions
- * Concerns of the effect of Long-period earthquake ground motions to high-rise and SI buildings
- * Earthquake occurrence probability is high for major subduction-zone earthquakes such as Nankai, Tonankai and Tokai earthquakes
- * Various projects on earthquake damage evaluations for subduction-zone earthquakes
- * MLIT funding for safety measures for long-period buildings (Selected Research Group + BRI)

Design earthquake motions for high-rise buildings 61



Design Motions Currently Used for Tall Buildings (>60m)

- 1. BSL Notification spectrum compatible motions (Fig.1)
- Modified Recorded motions (Vmax=25,50cm/s)
- 3. Site-specific motions

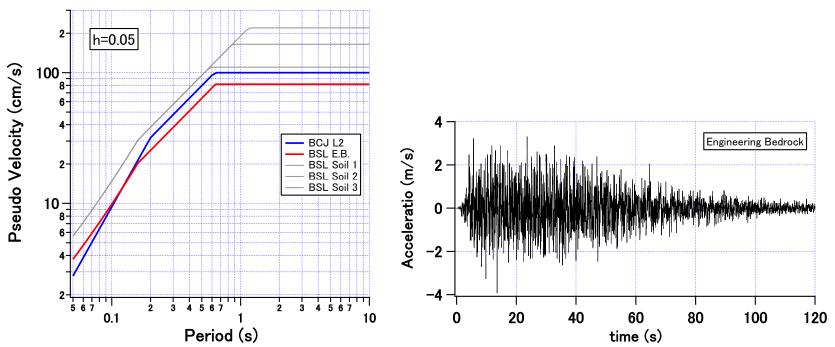


Fig.1 BCJ (L2) and BSL Design Spectra and BSL wave for Engineering Bedrock

Ground motion parameters and prediction model

1. Spectral Properties

1) Acceleration response spectrum (h=0.05, 0.01)

- 2) Energy Spectrum (h=0.10)
- 3) Site amplification coefficient
- 2. <u>Time history Properties</u>
 - 1) Site factors with phase properties controlling waveforms and duration time

Used Earthquake Data (Subduction, Crustal Eqs.)

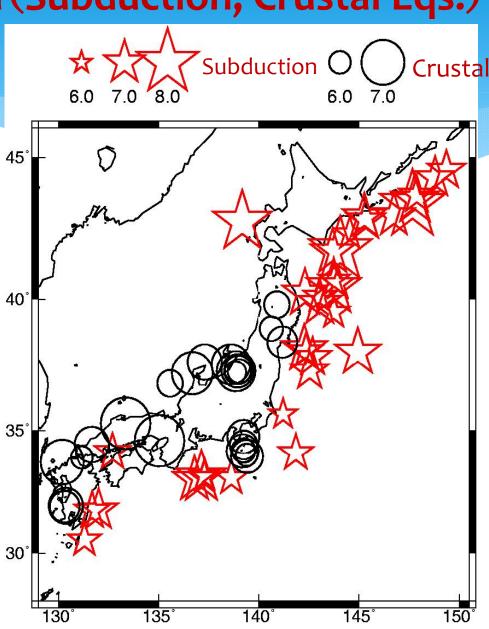
•Subduction:Mj≥6.5, Hypocentral dist.≤400km

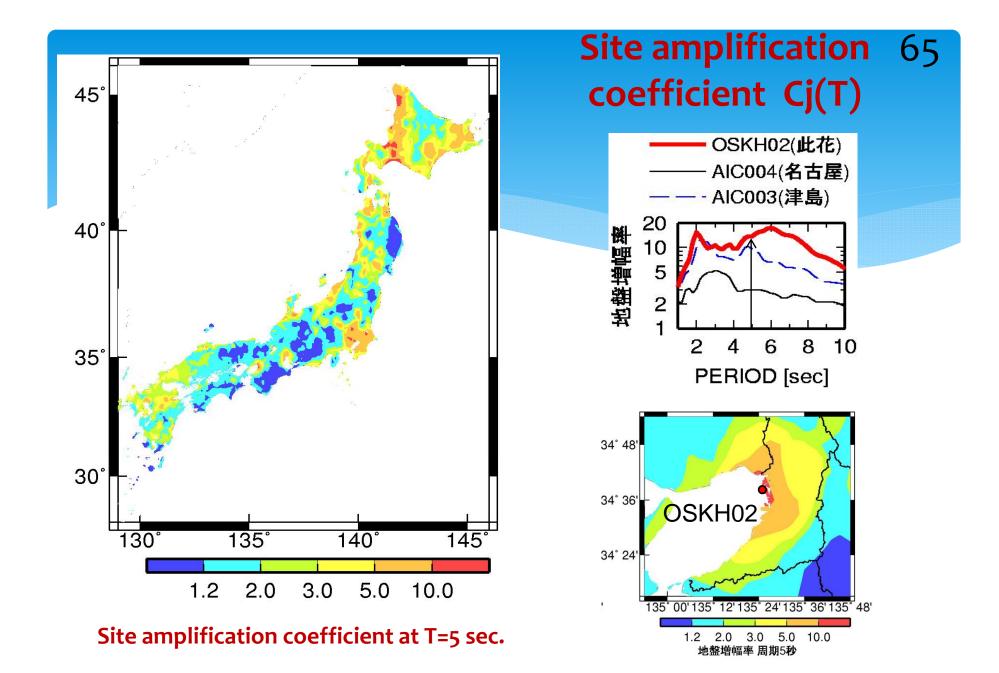
•Crustal:Mj≥6.0,

Hypocentral dist. ≦350km

•Focal depth≤60km Mj:JMA magnitude

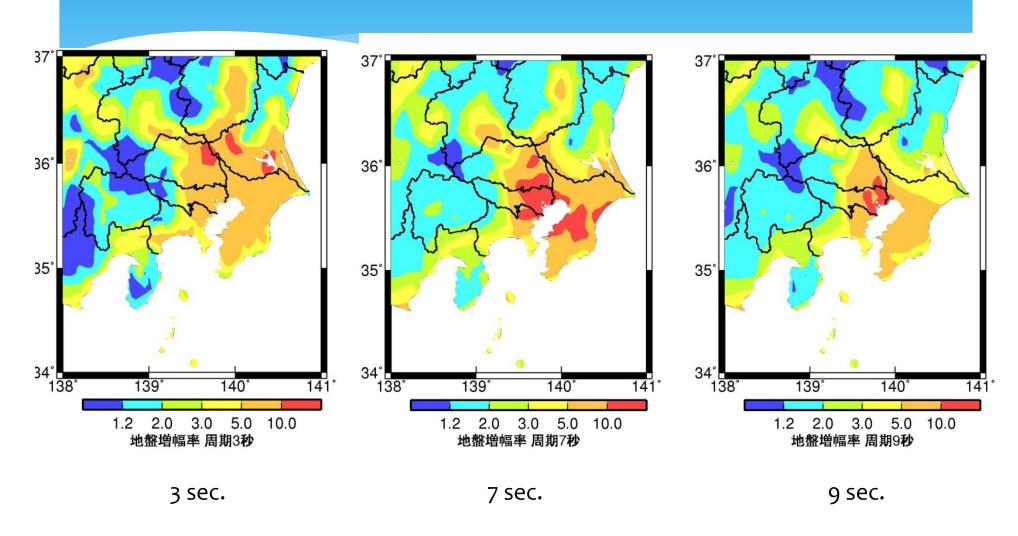
K-NET, KiK-net, JMA data were used in this study



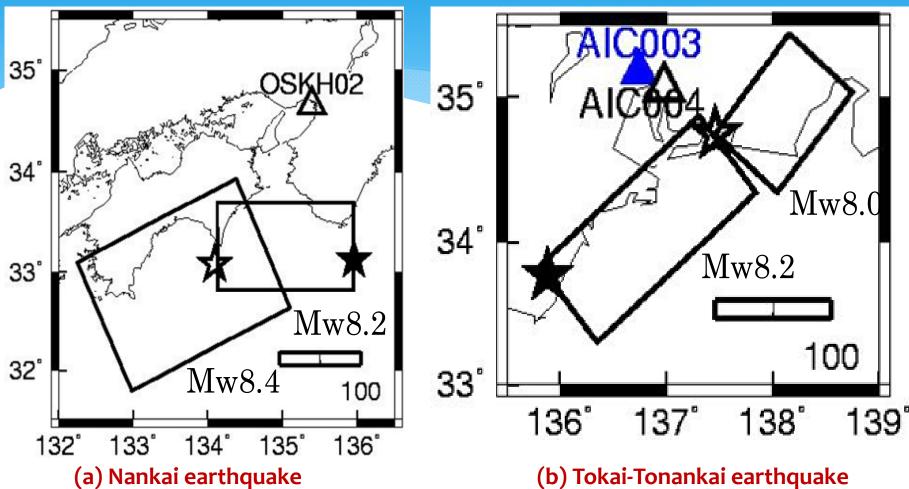


66

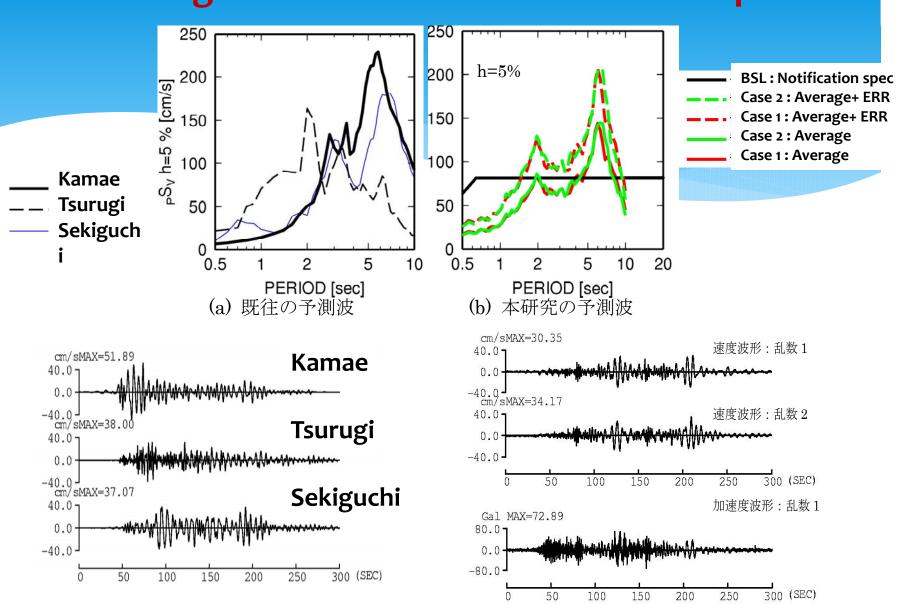
Site amplification factors for Sa(5%) horizontal components



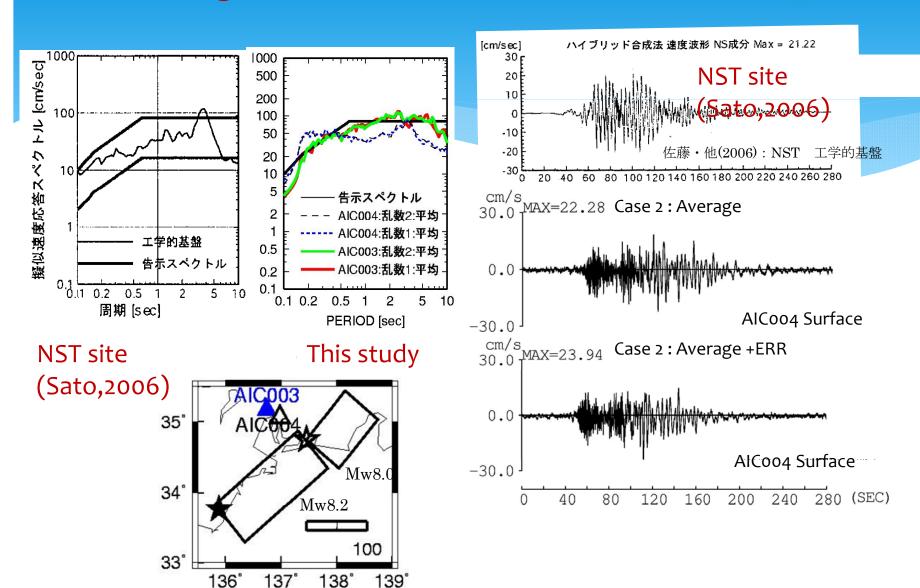
Simulated ground motion for large earthquakes



Simulated ground motion for Nankai earthquake⁶⁸



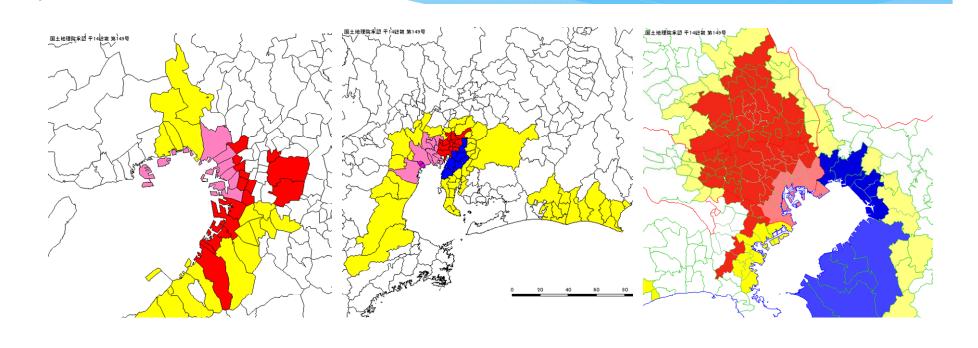
Simulated ground motion for Tonankai-Tokai earthquake 69



MLIT proposal for tentative measures for the safety of high-rise buildings

- * With MLIT funding, the methodology is constructed.
- * Long-period earthquake ground motions for specific sites can be evaluated including time histories.
- * Earthquake motions for verification generated for three major subduction-zone earthquakes
 - →Nankai, Tonankai and Miyagi-oki earthquakes
- * Long-period earthquake motions for 9 zoning sites in urban area were proposed for existing and new ones.
- * Public comments to this proposal were invited.
- * The 2011 Tohoku earthquake occurred.

Nine Zonings in Urban Areas

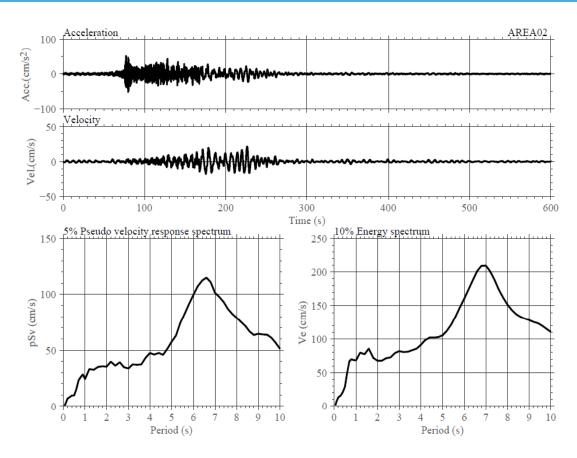


Osaka

Nagoya

Tokyo

Area 9 (representing Tokyo Bay area)



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End